

Problème 5.1

- * Méthode de Meyerhof
- * Pieu carré en béton
- * Battage

(a) Capacité en pointe

$$Q_P = m \times N \times A_P$$

$$Q_P = 400 \times 38 \times (0.3 \times 0.3)$$

$$Q_P = 1368kN$$

Capacité en friction

$$Q_F = n \times \bar{N} \times D \times A_S$$

$$Q_F = 2 \times 27 \times 15 \times (4 \times 0.3)$$

$$Q_F = 972kN$$

$$Q_{ult} = Q_P + Q_F = 2340kN$$

$$Q_{adm} = \frac{Q_{ult}}{F.S.} = \frac{2340}{4} = 585kN$$

(b) Tassement d'un seul pieu

$$Aire = 30cm \times 30cm = \frac{\pi}{4} D_{\acute{e}q}^2$$

$$D_{\acute{e}q} = 33.85cm$$

$$S_{1\ pieu} = \frac{D}{100} + \delta$$

$$S_{1\ pieu} = \frac{D}{100} + \frac{100 Q L_P}{EA}$$

$$S_{1\ pieu} = \frac{33.85}{100} + \frac{100 \times 585 \times 15}{(0.3)^2 \times \sqrt{30} \times 10^6 \times 5000} = 0.695cm \approx 0.7cm$$

(c) On vérifie d'abord l'espacement entre les pieux :

$$4m = 0.3m + 3S_H \Rightarrow S_H = 1.233m = 4.1D$$

$$3m = 0.3m + 2S_V \Rightarrow S_V = 1.35m = 4.5D$$

∴ On peut assumer que les pieux travaillent en groupe.

$$Q_{ult\ g} = Q_{ult\ s} \times N^{\circ} \text{ des pieux}$$

$$Q_{ult\ g} = 2340 \times 12 = 28080 \text{ kN}$$

$$Q_{adm\ g} = \frac{Q_{ult\ g}}{F.S.} = \frac{28080}{4} = 7020 \text{ kN (ou simplement } Q_{adm\ g} = 12 \times Q_{adm\ s})$$

$$S_g = S_s \sqrt{\frac{B}{b}} = 0.7 \sqrt{\frac{3}{0.3385}} = 2.084 \text{ cm}$$

Problème 5.2

* Bois

* Circulaire, $D=0.3\text{m}$

* F.S. de charge = 3.0

* $Q_{adm}=200\text{kN}$ (a) Capacité en pointe (pour $D<0.5\text{m}$, $N_c=9$)

$$Q_P = N_c \times c_u \times A_P$$

$$Q_P = 9 \times 60 \times \frac{\pi}{4} (0.3)^2$$

$$Q_P = 38.17\text{kN}$$

Capacité en friction

$$Q_F = \alpha \times c_u \times A_S = (\alpha \times c_u)_1 A_{S1} + (\alpha \times c_u)_2 A_{S2}$$

$$Q_F = 37 \times \pi(0.3) \times 8 + 46 \times \pi(0.3) \times L_2$$

$$Q_F = 278.973 + 43.354L_2$$

$$Q_{adm} = \frac{Q_P + Q_F}{F.S.} = 200\text{kN}$$

$$200 \times 3 = 38.17 + 278.973 + 43.354L_2$$

$$L_2 = 6.524\text{m}$$

$$L = 8 + 6.524 = 14.524\text{m} \quad \text{soit } L = 14.60\text{m}$$

Problème 5.3

* Pieu foré

* $D=0.3\text{m}$

(a) Capacité en pointe

$$Q_P = m \times N \times A_P$$

$$Q_P = 120 \times 45 \times \frac{\pi}{4} (0.3)^2$$

$$Q_P = 381.704\text{kN}$$

Capacité en friction

$$Q_F = n \times \bar{N} \times D \times A_S$$

$$Q_F = 1 \times 15 \times 10 \times (\pi \times 0.3)$$

$$Q_F = 141.372\text{kN}$$

$$Q_{ult} = Q_P + Q_F = 523.075\text{kN}$$

$$Q_{adm} = \frac{Q_{ult}}{F.S.} = \frac{523.075}{4} = 130.769\text{kN}$$

Problème 5.4

Formule de Hiley

$$Q_{ult} = \frac{W_r \times h \times e_h}{S + \frac{1}{2}(C_1 + C_2 + C_3)} \times \frac{W_r + n^2 W_p}{W_r + W_p}$$

* W_r = Poids du marteau; Marteau Vulcan 140C double actionDu tableau A-2, $W_r = 125 \text{ kN}$ * e_h = Efficacité du marteau

$$e_h = 0.78$$

* S = Enfoncement pour un coup (refus)

$$S = 19 \text{ mm}$$

* $W_r \times h$ = Énergie (du tableau) = 48.8 kN.m* W_p = Poids du pieu (Pieu tubulaire en acier)

$$W_p = \gamma \times \text{volume} = 77 (11045 \times 10^{-6} \times 16.76) = 14.25 \text{ kN}$$

* $C_1 = 0$

$$* C_2 = \frac{Q_{ult} \times 16.76 \times 10^3}{11045 \times 10^{-6} \times 2 \times 10^8}$$

* $C_3 = 2.5$ * $n = 0.5$

$$Q_{ult} = \frac{48.8 \times 10^3 \times 0.78}{19 + 0.5 \left(0 + \frac{16.76 Q_{ult}}{2209} + 2.5 \right)} \times \frac{125 + 0.5^2 \times 14.25}{125 + 14.25}$$

$$Q_{ult} = \frac{38064}{20.25 + 3.794 \times 10^{-3} Q_{ult}} \times 0.923$$

$$Q_{ult} = \frac{35142.57}{20.25 + 3.794 \times 10^{-3} Q_{ult}}$$

$$3.794Q_{ult}^2 + 20.25 \times 10^3 Q_{ult} - 35142.57 \times 10^3 = 0$$

$$Q_{ult} \approx 1379 \text{ kN}$$

$$Q_{adm} = \frac{Q_{ult}}{4} = 344.75 \text{ kN}$$